

SEL-121C PHASE DISTANCE/ TIME-OVERCURRENT RELAY GROUND DIRECTIONAL OVERCURRENT RELAY AND FAULT LOCATOR





- * ZONE 1 PHASE DISTANCE ELEMENT FOR INSTANTANEOUS TRIPPING
- * ZONE 2 PHASE DISTANCE ELEMENT CONTROLS TIME-OVERCURRENT ELEMENT TO COORDINATE WITH DOWNSTREAM DEVICES
- * REVERSIBLE ZONE 3 PHASE DISTANCE ELEMENT FOR DEFINITE TIME TRIPPING FOR REMOTE OR LOCAL BACKUP
- * RESIDUAL INSTANTANEOUS AND TIME-OVERCURRENT ELEMENTS
- * REVERSIBLE RESIDUAL DEFINITE TIME-OVERCURRENT ELEMENT FOR REMOTE OR LOCAL BACKUP
- * NEGATIVE- AND DUAL-POLARIZED ZERO-SEQUENCE GROUND DIRECTIONAL ELEMENTS
- * PROGRAMMABLE LOGIC FOR OUTPUTS, TRIPPING, AND RECLOSING
- * THREE-SHOT RECLOSING WITH SELECTABLE VOLTAGE SUPERVISION
- * FAULT LOCATING * EVENT REPORTING * METERING
- * AUTOMATIC SELF TESTING * RS232C COMMUNICATION

GENERAL DESCRIPTION

The SEL-121C PHASE TIME-DISTANCE RELAY AND GROUND DIRECTIONAL OVERCURRENT RELAY WITH FAULT LOCATOR provides high-speed and time-delayed phase and ground fault protection for transmission and distribution lines and cables. Zone 1 distance and high-set phase and directional residual-overcurrent elements provide fast Zone 2 phase and three-phase distance elements torque-control a operation. phase-time-overcurrent element to provide time-delayed tripping for faults beyond the reach of the zone 1. The phase time-current curve makes this relay especially easy to apply where coordination with protective devices at tapped load stations is required. The output of the zone 2 distance elements are also directly accessible for permissive overreaching transfer trip and other Zone 3 phase and three-phase distance elements may be set to applications. reach in the forward or reverse direction. For backup applications, a timer driven by the zone 3 elements is provided. The instantaneous and delayed A residual time-overcurrent element covers ground outputs are accessible. faults beyond the reach of the instantaneous overcurrent element and both its pickup and time-delayed response are accessible in the logic. A directionallysupervised residual-overcurrent element may be set to respond to forward or reverse direction faults and also drives a timer for backup.

Four types of time curves are provided for the phase and ground timeovercurrent elements: moderately inverse, inverse, very inverse, and extremely inverse. Different curve types may be selected for the phase and ground elements. Additionally, settings allow for the ground elements to be directional or nondirectional.

Loss-of-potential logic may be used to disable the mho elements whenever an unbalanced or balanced loss of potential condition exits, not associated with excessive current or current unbalance. It may also be used to cause the voltage-dependent ground-directional elements to default forward when a lossof-potential condition exists.

The relay elements and their timer outputs are combined in a 32-bit Relay Word. Logic, programmable by the applications engineer, combines these bits to control tripping, reclosing (initiation and cancellation), and four general programmable outputs.

A three-shot recloser is included that provides the user with three settable open interval timers, a reset timer, and voltage supervision. The reclosing initialization and closing conditions are easily defined by the applications engineer using the SET procedure.

Because of the many relay elements, the programmability of the SEL-121C relay, and its low cost, the SEL-121C relay meets the requirements of a broad spectrum of applications. The flexible yet simple programmability provides access to the relay elements (before and after time delays) and logic results, such as reclose initiate or cancel, loss of potential, alarm, and trip.

The SEL-121C Relay Function Block Diagram illustrates the basic configuration of the protective capabilities.

Analog inputs from current and voltage transformers are delivered to the protective relaying elements and saved for additional features, such as metering and fault locating.



The relay elements process the analog data. Some intermediate logic is performed, such as overcurrent supervision of the mho elements, directional supervision of the residual-overcurrent elements, and grouping of certain elements into zones.

The states of the intermediate results and some other information are recorded in the Relay Word.

Logic for tripping, closing, and other purposes use the Relay Word data. Most of that logic is programmable by logic masks.

APPLICATIONS

Transmission and Subtransmission Systems

The SEL-121C relay is ideal when the protection must coordinate with downstream apparatus, taps or buses equipped with time-current protection for phase and ground faults, yet must offer high-speed phase protection over as much of the line as possible.

Replacement of Outdated Protective Relays

The SEL-121C is the ideal relay to replace obsolete electromechanical relays. Its compact size and simple field wiring make replacement especially convenient in crowded substations. Its event-reporting and fault-locating features economically provide valuable engineering and operating information, eliminating the need for event recorders and oscillographs in most applications. Its instrument transformer burden is negligible.

Schemes Involving Communications

Although the SEL-121C relay was designed for applications at subtransmission voltages where communications are not usually applied, the relay supports direct and permissive underreaching transfer tripping, permissive overreaching transfer tripping, and blocking schemes. Since the event report shows the voltages, currents, relay elements, inputs and outputs, it is easy to evaluate scheme performance.

Backup Relaying

Where adequate high-speed primary protection already exists, the SEL-121C relay can be applied for backup. Its programmability and remote-access capabilities allow the relay settings to be adjusted remotely to meet virtually any contingency.

Its application also adds event reporting and fault locating.

Other Applications

The SEL-121C relay is also cost-effective in these applications: fault locating, temporary installations, bus-tie breaker relaying (where frequent setting changes may be required), and remote control and monitoring.

SPECIFICATIONS

Relay Functions

Mho characteristics for phase-phase and three-phase faults Zone 1: Instantaneous trip Zone 2: Controls phase time-overcurrent element Zone 3: Definite-time trip Residual-overcurrent protection for ground faults One instantaneous element Two definite-time elements One time-overcurrent element with selectable curve shapes Negative-and zero-sequence directional elements for ground faults. Zero-sequence element is dual polarized. Zone 3 mhos and the definite-time element may be reversed for local backup schemes or other applications. Automatic reclosing with voltage supervision for selectable fault types (3 shots).

Relay Elements

Phase overcurrent: 50AL, 50BL, 50CL (phase fault detectors) 50AH, 50BH, 50CH (high-set elements) 0.5 to 40 A pickup +/- 0.1 A +/- 2% of setting 51P phase time-overcurrent element. 1 - 12 A pickup setting, +/- 0.05A +/- 2% of settings above 3 A +/- 0.2A +/- 5% of settings below 3 A Three-phase and phase distance: 21ABC1, 21P1: 0.125 to 32 ohms 21ABC2, 21P2: 0.125 to 128 ohms 21ABC3, 21P3: 0.125 to 128 ohms Angle setting: 47 - 90 degrees in one degree steps. Zone 2 and 3 settings are limited as follows: For Zone 1 < 8 ohms: 1 - 16 times zone 1 For Zone 1 > 8 ohms: 1 - 4 times zone 1 Zone 2 may not be set greater than 4 times Zone 1 when Zone 3 is less than 4 times Zone 1. Mho elements operate in 10 - 45 ms (25 ms typical), including output relay delay. Steady-state Error: 5% of set reach +/- 0.01 ohm at angle of maximum torque for V > 5 V and I > 2 A. 10% of set reach +/- 0.01 ohm at angle of maximum torque for 5 > V > 1 V and 0.5 < 1 < 2 A. Transient Overreach: 5% of set reach, plus steady-state error.

Memory polarization: Zone 1, 2, and 3 three-phase elements are memory polarized using voltage from a four-cycle memory. Ground Overcurrent: 51N residual time-overcurrent element. Selectable curve shape (4 curves). Time dial: 0.50 to 15.00 in steps of 0.01 Pickup: 0.25 to 6.3 A, +/- 0.05 +/- 2% of setting. 50N1, 50N2, and 50N3 residual-overcurrent elements. Pickup: 0.2 to 47 times 51N pickup. Timers are provided for 50N2 and 50N3: Zone 2 Timer: 0-2000 cycles in 0.25 cycle steps Zone 3 Timer: 0-2000 cycles in 0.25 cycle steps Ground Directional Elements: Negative-sequence directional element: Angle: same as mho element setting. Zero-sequence directional element: Voltage polarization: Angle: same as mho element setting Voltage Polarization Sensitivities for 320 and 32V ***32V Sens. (VA) **320 Sens. (VA) *Z1 (ohms) 0.14 * 51N 0.04 / Z1 0.125 - 0.50.28 * 51N * Z1 0.14 * Z1 0.5 - 2.0 0.07 * 51N * Z1 0.04 * Z1 - 8.0 2.0 0.02 * 51N * Z1 0.01 * Z1 - 32.0 8.0 Z1 is the Zone 1 reach setting, in secondary ohms. 32Q sensitivity is in units of (neg. seq. amps) * (neg. seq. volts). 32V sensitivity is in units of (residual amps) * (Zero-sequence *** volts). Current polarization: Angle: Zero degrees. Sensitivity: (0.5 amps) * (51N pickup setting) in units of residual amps squared. Sequence-Component Elements: Zero-sequence overvoltage element (47NL) Pickup: 14 volts VO Zero-sequence overcurrent element (50NL) Pickup: 0.083 amps IO Positive-sequence overvoltage element (47P) Pickup: 14 volts Positive-sequence dead line threshold (47PXD) Pickup: User settable ($0 \le 47PXD \le 75V$), +/- 6% of setting Positive-sequence live line threshold (47PXL) Pickup: User settable ($0 \le 47PXL \le 75V$), +/- 6% of setting

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- Fault Location Fault location is computed from event reports stored following each fault. Algorithm compensates for prefault current for improved accuracy for high-resistance faults.
- Fault Reporting A data record is retained for each of the 12 most recent faults, which includes date, time, location, current, voltage, relay element, input contact and output contact information. The report may also be triggered by command or contact closure. When tripping occurs after the end of the event report, a second report is triggered at tripping.
- Self Testing Analog AC channel offset errors Stall timer monitors processor Power supply voltage checks Setting checks RAM, ROM, and A/D converter tests

Rated Input Voltage 115 volt nominal phase-to-phase, 3 phase 4 wire connection

- Rated Input 5 amps per phase nominal Current 15 amps per phase continuous 390 amps for one second thermal rating
- Output Contact 30 amp make per IEEE C37-90 para 6.6.2 Current 6 amp carry continuously MOV protection provided
- Logic Input 25 60 VDC for 48 VDC relays Ratings 60 - 200 VDC for 125 VDC relays 200 - 280 VDC for 250 VDC relays Current = 6 mA at nominal voltage
- Power Supply 48 Volt: 30 60 VDC; 12 watts 125 Volt: 200 VAC or VDC; 12 watts 250 Volt: 85 - 280 VDC or 85 - 200 VAC, 12 watts
- Dielectric Strength V, I inputs: 2500 VAC for 10 seconds Other: 3000 VDC for 10 seconds (excludes RS-232)

Interference IEEE C37-90 SWC test (type tested) Tests IEC 255-6 interference test (type tested)

Impulse Tests IEC 255-5 0.5 joule 5000 volt test (type tested)

RFI Tests Type-tested in field from a 1/4-wave antenna driven by 20 watts at 150 MHz and 450 MHz, randomly keyed on and off, at a distance of 1 meter from relay.

Dimensions 5 1/4" x 19" x 13". Mounts in standard 19" relay rack. Also available for vertical mounting.

Unit Weight 21 pounds

Operating -20 deg C to + 55 deg C Temperature

Burn-in 60 deg C for 100 hours Temperature

Basic Protective Capabilities

The SEL-121C relay provides complete protection for transmission line faults of all types.

Phase-to-Phase and Three-Phase Faults:

Three zones are provided. Zones 1, 2, and 3 are mho circles passing through the origin. Zone 3 may be reversed. The instantaneous outputs of all three elements are available. The zone 2 elements torque-control a phase timeovercurrent element, making it possible to coordinate zone 2 operations with downstream time-current devices. The zone 3 elements control a timer, so that a definite-time-delay output is available for local or remote backup.

The three-phase elements are supervised by three overcurrent elements, which must all pick up. Four-cycle memory polarization is provided for zones 1, 2, and 3.

The phase-to-phase characteristics are mho, based on the compensator-distance principle. They have no response for three-phase faults. They are supervised by three overcurrent elements. At least one overcurrent element must pick up to enable the phase-to-phase mho elements. They are also supervised by a lossof-potential scheme, when enabled.

Three high-set nondirectional overcurrent elements provide backup to the threephase and phase-to-phase mho elements. They are nondirectional.

Ground Faults:

Ground fault protection consists of an instantaneous residual-overcurrent element, a time-overcurrent element, and two definite time elements.

Direction is determined by a negative-sequence directional element, and a dualpolarized zero-sequence element. Settings are provided to select the negativesequence element, or neither, either or both sources of zero-sequence polarization. When voltages are lost, the direction is assumed forward. To securely discriminate between forward and reverse-direction faults, the directional elements have a torque threshold which must be exceeded in either direction before the fault direction is declared.

The direction of the 50N3 residual-overcurrent element may be reversed, to assist in local backup and in weak-infeed schemes.

The curve shape of the time-overcurrent element is user-selectable. This element is either nondirectional or forward-reaching, as enabled.

Switch-Onto-Fault Protection:

The high-set overcurrent elements will respond to a zero-voltage three-phase fault at any time. The four-cycle memory polarization of the three-phase elements guarantees positive action for four cycles when bus-side voltages are used.

The 52BT timer and the MTO mask may be used to select relay elements (such as the Zone 2 distance element or the pickup of the sensitive overcurrent elements) for instantaneous tripping, until a short time after the breaker is closed.

Reclosing:

A three-shot reclosing relay is provided. Reclosing may be initiated or cancelled for any of the relay elements in the Relay Word.

Voltage supervision is provided in the reclosing logic. The SEL-121C reclosing relay provides multi-shot reclosing for dead voltage, live voltage, or no voltage supervision. The voltage conditions must be satisfied to initiate the open interval timer (7901) and to assert a close contact. An option is provided through the setting procedure (CVC) to require voltage supervision to initiate the open interval timer, but to allow closing regardless of the voltage conditions at close time. The voltage supervision can be specified to be satisfied on the first shot only, or on all shots using the VSA setting in the SET procedure.

The reclosing relay in the SEL-121C uses user-settable timers to ensure a finite reclosing time. A voltage condition timer (VCT) defines the maximum time allowed for the supervising voltage conditions to be met. If the voltage conditions are met for one cycle before the expiration of VCT timer, a successful voltage condition is declared and the open interval timer (7901) is allowed to run. At the expiration of the open interval timer, the supervisory requirements for closing are checked against the existing voltage conditions, and if satisfied, the close contact is asserted.

LOGIC DESCRIPTION

Relay Elements

Single-phase overcurrent relays High-set single phase OC relays	50AL 50BL 50CL 50AH 50BH 50CH	(phase fault detectors)
Zone 3 three-phase mho distance	21ABC3	(reversible)
Zone 3 line-line mho distance	21P3	(reversible)
Zone 2 three-phase mho distance	21ABC2	torque-controls 51P
Zone 2 line-line mho distance	21P2	torque-controls 51P
Zone 1 three-phase mho distance Zone 1 line-line mho distance	21ABC1 21P1	

Phase time-overcurrent pickup	51PP	T.C. by 21ABC2, 21P2
Phase time-overcurrent trip	51PT	T.C. by 21ABC2, 21P2
Residual time-overcurrent pickup	51NP	T.C. or nondirectional
Residual time-overcurrent trip	51NT	T.C. or nondirectional
Residual inst-overcurrent	50N1	nondirectional
Residual inst-overcurrent	50N2	nondirectional
Residual inst-overcurrent	50N3	nondirectional
Negative-sequence directional Zero-sequence dual pol directional Zero-sequence overvoltage Zero-sequence overcurrent Positive-sequence overvoltage Positive-sequence voltage-aux	32Q 32D 47NL 50NL 47P 47PXD	32QF=forward; 32QR=reverse 32DF=forward; 32DR=reverse 14 V Vo (loss-of-pot det) 83 mA Io (loss-of-pot det) 14 V V+ (loss-of-pot det) Dead voltage detector (if VposLL \leq 47PXD => dead voltage)
Positive-sequence voltage-aux	47PXL	Voltage) Live voltage detector (if VposLL ≥ 47PXL => live voltage

Contact Inputs

Direct trip	DT
Permissive trip	PT
Block trip	BT
Direct close	DC
Circuit breaker monitor	52A
	EXT

Contact Outputs

Circuit breaker trip	TRIP
Circuit breaker close	CLOSE
Programmable output 1	A1
Programmable output 2	A2
Programmable output 3	A3
Programmable output 4	A4
System alarm	ALARM

INTERMEDIATE LOGIC

The logic equations developed below represent combinations of the relay elements and other conditions.

Set LOP	= 47NL * NOT (50NL)	(Zero sequence set condition includes a three-cycle pickup
	+ NOT (47P) * NOT (50L)	delay.)

Clear LOP = NOT (47NL) * 47P + NOT (LOPE)

(The different set and clear conditions ensure LOP stays latched during subsequent faults, but is cleared when balanced voltages and currents return.)

50L = 50AL + 50BL + 50CLphase fault current supervision 3P50 = 50AL * 50BL * 50CL three-phase fault current supervision 50H = 50AH + 50BH + 50CH high-level overcurrent condition Z3ABC = 21ABC3 * 3P50 * NOT (LOP)(3ABC in relay word) Z2ABC = 21ABC2 * 3P50 * NO1 (LOP)(2ABC in relay word) Z1ABC = 21ABC1 * 3P50 * NOT (LOP)(IABC in relay word) $Z3P = 21P3 \times 50L \times NOT (LOP)$ Z2P = 21P2 * 50L * NOT (LOP) Z1P = 21P1 * 50L * NOT (LOP)DF = (320F + LOP) * 320E + 320F * 321E +(32DF + LOP) * 32VE + NOT(32QE + 32VE + 32IE) forward direction DR = 32QR * 32QE + 32DR * (321È + 32VE) reverse direction if Zone 3 is forward if Zone 3 is reverse D3 = DF D3 = DR67N1 = 50N1 * DFT.C. 67N2 = 50N2 * DFT.C. 67N3 = 50N3 * D3T.C. reversible NOTE: When directional elements are all disabled (32QE = 32VE = 32IE = N), the DF (directional forward) bit defaults forward. The Zone 3 ground element will not operate under this condition if Zone 3 = R. Z2GT = 67N2 + Z2GTMRzone 2 timeout-ground Z3PT = (Z3P + Z3ABC) * Z3PTMRzone 3 timeout-phase $Z3GT = 67N3 \times Z3GTMR$ zone 3 timeout-ground

<u>RELAY WORD</u>

Relay elements and intermediate logic results are represented in a 32-bit relay word (grouped into four 8-bit words). The user selects bits in this word to perform the desired functions for controlling outputs and for initiating or cancelling reclose. The selected bits are stored in masks for each function. The user programs the bits in these masks with the LOGIC command.

Relay Word:

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51PT	1ABC	2ABC	3ABC	51PP	50H	50L	LOP
51NT	67N1	67N2	67N3	51NP	ZIP	Z2P	Z3P
DF	DR	Z 2 GT	Z3GT	3P50	RC	RI	Z3PT
ALRM	TRIP	TC	DT	52BT	52AT		

The meaning of each bit of the relay word is explained in the Relay Word Bit Summary Table listed below.

SEL-121C RELAY WORD BIT SUMMARY TABLE

	-	Phase time-overcurrent trip Zone 1 three-phase mho distance element Zone 2 three-phase mho distance element Zone 3 three-phase mho distance element Phase time-overcurrent pickup
50H 50L LOP	-	High set instantaneous overcurrent element Low set instantaneous overcurrent element Loss of potential element
51NT 67N1 67N2 67N3 51NP Z1P Z2P Z3P		Zone 1 phase-phase mho element Zone 2 phase-phase mho element
DF DR Z2GT Z3GT 3P50 RC RI Z3PT	- - -	Zone 3 timeout-ground Three-phase overcurrent element Reclose cancellation Reclose initiation
ALRM TRIP TC DT 52BT 52AT		Circuit breaker trip Trip (OPEN) command

The use of the relay word and programmable masks provides the user with great flexibility in applying the SEL-121C relay, without rewiring panels or changing jumpers on circuit boards.

OUTPUT EQUATIONS

The logic for controlling the TRIP, A1, A2, A3, and A4 output relays is programmable for flexibility and for testing. The logic is programmed by setting masks for various conditions, which are applied to the general relay flag word. The general forms for each of the output equations follow:

Let R = relay word

MTU = mask for trip (unconditional) MPT = mask for trip (permissive trip) MTB = mask for trip (with no blocking) MTO = mask for trip (with breaker open) then: TRIP = R * MTU + R * MPT * PT + R * MTB * NOT (BT) + R * MTO * 52BT close TRIP - TRIP open TRIP = NOT (TRIP) * NOT(52A) * (60 ms minimum TRIP) close CLOSE = (DC + 790I1 + 790I2 + 790I3 + Close Command) * NOT (52A) open CLOSE = NOT (CLOSE) + 79RS AI = R * MA1 A2 = R * MA2 A3 = R * MA3 A4 = R * MA4

The "*" symbol indicates logical "and", the "+" indicates logical "or", and the 7 indicates exclusive "or".

RECLOSING RELAY

The reclosing relay provides up to three shots of automatic reclosing for selectable fault types. The three open intervals and the reset timer are individually programmable and voltage supervision can be employed.

To provide flexibility in applying the SEL-121C relay to various reclosing schemes, the conditions for reclose initiation and cancellation are selected in a similar way to the programming of the output relays:

RI = R * MRIRC = R * MRC

where MRI is the mask for reclose initiation, and MRC is the mask for reclose cancellation.

The SEL-121C relay has the option for voltage supervision of the reclosing function. The voltage supervision can be selected to reclose on live voltage, dead voltage or can be disabled. These conditions, as well as 47PX thresholds to define live voltage/dead voltage conditions are fully user-selectable using the SET procedure. For example, to reclose only for all Zone 1 faults, and to supervise the reclose with a dead voltage condition, the following would be representative settings:

47PXD = 10	This define	s the	positive	sequence	dead	voltage	threshold
	as 10kV pha	ise-to	-phase.	•		-	

- VCT = 100 The voltage condition timer insures that the reclosing relay has a finite time in which to satisfy the supervising voltage conditions. VCT defines the maximum time allowed for the supervising voltage conditions to be met. VCT begins timing after the trip unasserts and the breaker opens, as indicated by the 52A contact.
- LLC = N Disables live voltage supervision.

- DLC = Y Enables dead voltage supervision.
- CVC = Y When CVC is enabled, voltage supervision is required to begin the open interval timer, and voltage supervision is required at the expiration of the open interval timer to close.
- VSA = Y Enables voltage supervision for all shots. If VSA = N, only the first shot is supervised, with subsequent shots being unsupervised.

MRI: 40 44 00 00	roclosing will	for reclose initiation, is set so that be initiated only for Zone 1 phase and This is done using the "LOG MRI" command.
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The SEL-121C relay voltage supervision logic assumes line side PT's for live voltage/dead voltage supervision. There are no capabilities provided in this relay for line side/bus side checking or sync-check.

The following timing diagrams illustrate the above settings in a reclosing sequence. A first shot with dead voltage supervision is shown in all timing diagrams. The second shot illustrates some of the features of the SEL-121C reclosing relay.

Timing diagram TD1 shows the first shot of the dead voltage supervised reclose followed by a cancelled second shot. The failure of the second shot to reclose is due to the supervising voltage conditions remaining unsatisfied during the voltage condition timer period. In this case, the positive sequence voltage, V+, does not decay, and therefore the magnitude of V+ is greater than the positive sequence dead voltage threshold, 47PXD. This condition remains throughout the duration of the voltage condition timer, VCT. At the expiration of VCT, reclosing is cancelled due to voltage supervision. If, at any time during the duration of the voltage condition timer, the positive sequence voltage decays such that it is less than 47PXD and remains in this state for one power system cycle, the voltage condition would have been declared valid and the open interval timer run.

Timing diagram TD2 illustrates, again, a first shot, followed by a cancelled second shot due to voltage supervision. This diagram shows a reclose cancellation due to an unsatisfactory voltage condition at close time. The supervising voltage conditions were satisfied and the open interval timer was run. At expiration of the open interval timer (790I), the voltage conditions are checked before the close contact is asserted. The voltage conditions are not satisfied, and the reclosing sequence is cancelled.

Timing diagram TD3 shows identical system conditions to those of TD1, but with a setting change that allows a successful reclose on the second shot. If VSA=N, only the first shot will have voltage supervision.

Timing diagram TD4 shows identical system conditions to those of TD2, but with no voltage supervision required at close (CVC = N). The supervising voltage conditions are met to start the open interval timer, but are not required to assert the close contact.



Timing diagram showing the first shot of a dead voltage supervised reclose, followed by a cancelled second shot due to bad voltage conditions not allowing the open interval timer to begin.

TIMING DIAGRAM TD1

DWG. NO. A7-0421 DATE: 10-19-88



Timing diagram showing the first shot of a dead voltage supervised reclose, followed by a cancelled second shot due to bad voltage conditions at close.

TIMING DIAGRAM TD2

DWG. NO. A7-0422 DATE: 10-19-88

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Timing diagram showing the first shot of a dead voltage supervised reclose, followed by a second shot. Voltage supervision is only required for the first shot by setting VSA=N.

TIMING DIAGRAM TD3

DWG. NO. A7-0423 DATE: 10-19-88

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Timing diagram showing the first shot of a dead voltage supervised reclose, followed by a second shot. Voltage supervision is not required at close by setting CVC=N.

TIMING DIAGRAM TD4

DWG. NO. A7-0424 DATE: 10-19-88 The above illustrates the use of the SEL-121C voltage supervised reclosing relay for a dead voltage application. An analogous group of settings can be defined for an equally flexible live voltage application.

The following logic equations define the SEL-121C relay reclosing function:

- RECLOSE INITIATION

RI = R * MRI

- RUN OPEN INTERVAL TIMER 7901 WITH VOLTAGE SUPERVISION

VI = (LLC * 47PXL) + (DLC * $\overline{47PXD}$) + \overline{VSUP} VSUP = (LLC \oplus DLC) * [(\overline{VSA} * \overline{SHOT}) \oplus VSA]

- RECLOSING CANCELLATION WITH VOLTAGE SUPERVISION

 $RC_v = (R * MRC) + 79RS_{exp} + wtim_{exp} + VCT_{exp}$

- RECLOSE TRIPPED BREAKER

Reclose = $RI_v * \overline{RC_v} * VC *790I_{exp}$ VC = (DLC * $\overline{47PXD}$) + (LLC * 47PXL) + \overline{VSUP} + CVC

Where

R : MRI : LLC : DLC : 47PXL: 47PXD: VSUP : VSA : SHOT : RCv : 79RS : MRC : VCT : wtim : CVC :	Positive sequence voltage - dead voltage Voltage supervision required for this shot All shots require voltage supervision Shot counter - zero relative Reclose cancel with voltage supervision Reclosing reset timer Reclose cancel mask Voltage condition time Thirty-second timer for external close Check voltage at close
CVC : 7901 :	Check voltage at close

The reclose initiation and cancellation due to the logic masks (R * MRI, R * MRC) are only applicable during the time for which the trip output is asserted. For example, if reclosing is not initiated before the trip output unasserts, then the reclosing function will be locked out and no reclose will occur.

The open intervals do not begin until the TRIP output unasserts and any supervising voltage conditions are met. Since the TRIP output never asserts for less than 60 ms and the voltage condition may take a finite time to be satisfied, the open interval may start several milliseconds after the fault has actually cleared and the breaker opened.

Reclose is automatically cancelled when the circuit breaker is observed to trip when a fault condition is not present, or if a fault occurs.



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SEL-121C VOLTAGE **SUPERVISED** THREE SHOT RECLOSING LOGIC

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SETTING PROCEDURE

The SET command invokes the relay setting procedure. Each setting is presented and prompted for in turn. If a new setting value is desired, it is entered in response to the appropriate prompt, while just pressing carriage return retains the old setting and prompts for the next one.

In the example shown, only the XO value was changed. It was changed from 159.69 to 143.07. Note that the new value of 143.07 is presented at the end of the procedure before enabling, along with all other settings. This provides a final inspection for typographical or other errors.

As a convenience, the user could have typed END in response to the prompt for Line Length (or any other setting except Relay ID), and gone directly to the final presentation of settings, without having to scroll through the rest of the prompts.

=>SET

SET clears events. CTRL-X cancels. Enter data, or RETURN for no change

ID : Example 69kV Line ?	
R1 : (Ohms pri) = 49.83 X1 : = 56.32 R0 : = 56.07 X0 : = 159.69 LL : Line Length (mi) = 60.00	? ? ? ? 143.07 <-operator changes XO ? <- could type END here
CTR : = 60.00 PTR : = 600.00 MTA : Max Torque Angle (deg) = 49.00 LOCAT: Locate faults (Y/N) = Y	? ? ?
47PXD: Dead volts (kV ph-ph). = 10.00 47PXL: Live volts = 25.00 VCT : Volt cond timer (cyc). = 100.00	? ? ?
LLC : Live check only (Y/N). = N DLC : Dead check only = N CVC : Supervise at close = Y VSA : V sup all shots = N	? ? ?
790I1: Open Int 1 (cyc) = 40.00 790I2:	? ? ? ? ? ? ? ? ? ? ? ? ? ? ? ? ? ? ? ?
50H: PU= 1500.00Z1%: Reach (% line)= 80.00Z2%:= 120.00Z3%:= 150.00Z3DP: Dly-Phase (cyc)= 60.00	? ? ? ?

51PP : PU (Amps pri).... = 120.00 ? 51PTD: Time Dial..... = 3.00 ? 2 51PC : Curve (1,2,3,4) = 2 ? 51NP : PU (Amps pri).... = 100.00 ? 51NTD: Time Dial..... = 2.00 ? 51NC : Curve (1,2,3,4) = 3 ? 51NTC: Torque Ctrl (Y/N).... = Y 50N1P: PU (Amps pri).... = 403.00 ? ? 50N2P: = 288.00 ? 50N3P: = 237.00 ? Z2DG : Dly-Gnd (cyc)..... = 20.00 Z3DG : = 40.00 ? ? 52BT : Dly (cyc)..... = 30.00 ? ZONE3: Dir (F=fwd,R=rvs).... = F ? 32QE : Enable (Y/N)..... = N ? 32VE : Y 32IE : = Y ? ? LOPE : Loss of Pot (Y/N).... = Y ? TIME1: Port 1 timeout (min).. = 5 TIME2: = 0 ? 2 AUTO : Auto port (1,2,3).... = 2 RINGS: (1-30).... = 3 2 New settings for: Example 69kV Line X0 =143.07 LL =60.00 =56.07 X1 =56.32 RO R1 =49.83 MTA =49.00 CTR =60.00 LOCAT=Y PTR =600.00 VCT =100.00 47PXD=10.00 47PXL=25.00 CVC =Y VSA =N DLC =N LLC =N 79RS =240.00 50L =50.00 79013=80.00 79012=60.00 790I1=40.00 Z3DP = 60.00Z2% =120.00 Z3% =150.00 Z1% =80.00 50H =1500.00 51PC =2 51PP =120.00 51PTD=3.00 51NTC=Y 51NTD=2.00 51NC = 351NP =100.00 50N2P=288.00 Z2DG =20.00 Z3DG = 40.0050N1P=403.00 50N3P=237.00 52BT =30.00 ZONE3=F 32QE =N 32VE -Y 321E =Y TIME1=5 TIME2=0 AUTO =2RINGS=3 LOPE =Y OK (Y/N) ? Y Please wait... Enabled The following data are required to set the relay: Pos. seq. primary impedance of line (0-9999 ohms) R1, X1 н " (0-9999 ohms) R0, X0 Zero seq. Line length (0.1-999 miles) LL CT ratio (e.g. for 600/5, enter 120) (1-5000) PT ratio (e.g. 1200/1, enter 1200) (1-10,000) CTR PTR Maximum torque angle for mho elements (47-90 degrees) MTA Do you want the fault locator enabled? (Y or N) LOCAT

47PXD Pos. seq. ph-ph voltage threshold for dead voltage (0-2000 kV) 47PXL Pos. seq. ph-ph voltage threshold for live voltage (0-2000 kV) VCT Voltage condition timer defines maximum time for the supervising voltage conditions to be met (0-10,000 cycles) LLC Live voltage supervision enabled? (Y or N) DLC Dead voltage supervision enabled? (Y or N) Check voltage at close? (Y or N) CVC VSA All shots supervised? (Y or N) Note: N implies only the first shot has voltage supervision. All subsequent shots are unsupervised. Reclosing relay open interval 1 (1/4 to 10,000 cycles; 0 disables)79011 reclosing) 79012 Reclosing relay open interval 2 (1/4 to 10,000 cycles; 0 disables reclosing) 79013 Reclosing relay open interval 3 (1/4 to 10,000 cycles; 0 disables reclosing) 79RS Reclosing relay reset time (60 to 8,000 cycles) Phase overcurrent element low pickup (0.25-50,000 primary amperes) 50L Phase overcurrent element high pickup (0.25-50,000 primary amperes) 50H Z1% Zone 1 reach (percent of line length: 0 to 2000%) Z2% Zone 2 reach (percent of line length: 0 to 3200%) Zone 3 reach (percent of line length: 0 to 3200%) Z3% Zone 3 delay for phase and three-phase faults (0-2000 cycles in 1/4Z3DP cycle steps) Phase time-overcurrent pickup (1-50,000 primary amperes) 51PP Phase time-overcurrent time dial (0.5-15) 51PTD 51 PC Phase time-overcurrent curve index. Choices are as follows: Use 1 to select a moderately inverse curve Use 2 to select an inverse curve Use 3 to select a very inverse curve Use 4 to select an extremely inverse curve 51NP Residual time-overcurrent pickup (0.25-50,000 primary amperes) 51NTD Residual time-overcurrent time dial (0.5-15) Residual time-overcurrent curve index. Choices are as follows: 51NC Use 1 to select a moderately inverse curve Use 2 to select an inverse curve Use 3 to select a very inverse curve Use 4 to select an extremely inverse curve Do you want residual time-overcurrent torque control? (Y or N) 51NTC 50N1P Zone 1 residual instantaneous overcurrent (0.25-50,000 primary amperes) Zone 2 residual instantaneous overcurrent (0.25-50,000 primary amperes) Zone 3 residual instantaneous overcurrent (0.25-50,000 primary amperes) 50N2P 50N3P Zone 2 delay for ground faults (0-2000 cycles in 1/4 cycle steps) Z2DG Zone 3 delay for ground faults (0-2000 cycles in 1/4 cycle steps) Z3DG

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- 52BT 52B time delay (0 to 10,000 cycles)
- ZONE3 Zone 3 direction (F = forward or R = reverse)
- 32QE Do you want negative sequence directional supervision of the ground overcurrent elements? (Y or N)
- 32VE Do you want voltage polarization for the zero sequence directional element enabled? (Y or N)
- 32IE Do you want current polarization for the zero sequence directional element enabled? (Y or N)

LOPE Should tripping be blocked when loss of potential is detected? (Y or N)

- TIME1 Timeout for Port 1 (0-30 minutes)
- TIME2 Timeout for Port 2 (0-30 minutes)
- AUTO Autoport (port 1, 2, or 3 (for both))
- RINGS The number of rings after which the modem answers (1-30 rings)

As you enter the settings, they are checked against the setting limits given above. Then the relay computes internal settings from your entries, and checks them to ensure they are within the range of the relay.

For example, let CTR=1000 and 50N1P = 1. Each of these settings is admissible alone, but together they result in a secondary pickup setting of 1 mA, which is out of range. Internal setting error messages indicate such conditions after you select to enable the new settings.

The zone 1, 2, and 3 reach values are the reaches of the mho units for a zero-resistance fault on the transmission line. The maximum torque angle (MTA) for the mho circles is independently set, and the diameter of the circle is expanded to keep the reach setting in the direction of the transmission line impedance constant as the maximum torque angle is separated from the transmission line angle. Thus, the maximum torque angle setting does not affect the reach in the direction of the transmission line, and the mho circle diameter relates to the set reach and the difference between the transmission line angle and the MTA by the expression below.

DIAMETER = [SET REACH] / [cos (T. L. ANGLE - MTA)]

Example 69 kV Line

Date:

FID=SEL-121C-R100-V656mptr-0881004

F10=5EL-121	C-KIU	0-49200)(F-DQ	01004						
		rrents ampa)				Voltage (kV)	9	Relays	Qutputs	Inputs
TPOL	IR	1A	IB	10	VA	VB	VC		TCAAAAA PL1234L	
0 0 0 0	-1 1 1 0	64 - 102 - 64 102	57 106 -57 106	- 121 - 6 121 6	21.6 -33.9 -21.5 33.8	18.6 35,6 -18,6 -35,6	-40.2 -1.8 40.2 1.8	L		····*·
0 0	-2 0 2 -1	64 102 -63 101	57 106 -57 106	-121 -6 121 6	21.6 -33.8 -21.6 33.9	18.6 35.6 -18.6 -35.6	-40.2 -1.8 40.2 1.8	L		····
0 0	-1 1 1 -1	63 -101 -64 102	57 106 -57 106	- 121 -6 121 6	21.6 -33.9 -21.6 33.8	18.6 35.6 -18.6 -35.7	-40.2 -1.8 40.3 1.7	L L		····*·
0 0 -1	-1 52 72 61	64 -35 -217 -24	57 78 - 40 - 29	- 121 6 85 - 9	19,9 -31,1 -17,0 26,6	18.2 36.9 -18.1 -38.3	-40.7 -0.4 40.9 -1.2	L K		····*·
0 0-5	44 17 56 13	460 14 -562 -12	13 4 •2 0	-28 1 5 0	15.7 -24.5 -15.4 24.2	18.5 38.7 -18.6 -38.8	-40.6 1.7 40.5 -1.7	L.31P.	•	····*·
0 0-5	71 13 74 12	575 11 -576 -12	0 0 0 0	-1 -1 1	15.4 -24.2 -15.3 24.2	18.6 38.8 -18.6 -38.8	-40.5 1.7 40.5 -1.8	L.31P. L.31P.	*.*.* *.*.* *.*.*	
0 0 -5	74 12 74 12	577 12 -577 -12	0 0 0	-1 -1 1	15.3 -24.2 -15.3 24.2	18.6 38.8 -18.6 -38.8	-40.5 1.8 40.5 -1.8	L.31P. L.31P.	*.*.* *.*.* *.*.*	
0 0-5	74 12 74 12	577 12 577 -12	0 0 0	-1 -1 1	15.3 -24.2 -15.3 24.2	18.6 38.8 -18.6 -38.6	-40.5 1.8 40.5 -1.8	L.31P. L.31P.	*,*,*,, *,*,*,, *,*,*,,	
0 0 -5	74 12 74 12	577 12 577 -12	0 0 0	-1 0 0	15.3 -24.2 -15.3 24.2	18.6 38.8 -18.6 -38.8	-40.5 1.8 40.5 -1.8	L.31P. L.31P.	*.*.* *.*.* *.*.*	
0 0 -5	74 12 74 12	577 12 -577 -11	0 0 0 0	-1 1 1 -1	15.3 -24.2 -15.3 24.3	18.6 38.8 -18.6 -38.7	-40.5 1.8 40.5 -1.7	L.31P. L.31P.	*,*,*,, *,*,*,, *,*,*,,	
0 - 0 -4	74 40 01 52	576 -40 -403 51	0 0 0	0 -1 1 1	17.0 -27.0 -19.8 31.0	19.0 37.5 -19.1 -36.6	-40.0 0.5 39.8 0.5	L.31P.	*,*,*,, *,*,*,, *,*,*,,	
Event : 1 Duration: 7		Locatio flt Cur		29.97 576.8	mi 3.	.76 ol	wis sec			
R1 +49.83 CTR =60.60 479XD=10.60 LLC =N 79011=40.60	P1 47 D1 75	(R =600 /PXL=25. .C =N /012=60.	00 .00	NTA = VCT = CVC = 79013=			=N =240.00	5 SQL		
50H =1500. 51PP =120.0 51NP =100.0 50N1P=403.0 52B1 =30.00 LOPE =Y	0 51 0 51 0 50 20	17 = =80. PTD=3.0 NTD=2.0 N2P=286 NE3=F NE1=5	10 10	51PC =	3 237.00 N	51NT(+20.00 =¥			
Logic settin	Ngs:									

NTU	HPT	MTB	MTO	HAT	MA2	MA3	MA4	MRI	MRC	
C4	E4	00	F4	E4	80	00	00	00	F5	
C4	E6	00	E7	E6	80	00	DO	44	80	
31	31	00	31	20	00	02	04	00	31	
30	00	00	30	00	00	00	00	00	30	

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EXPLANATION OF EVENT REPORT

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Example	69kV Li	ne			I	Date: 13	2/7/87	Time: 15:12:24.658		
	C	urrents			•	Voltage: (kV)	\$	Relays Outputs inputs		
		(amps)						522655 TCAAAAA DPBDSE		
1POL	18	14	18	10	¥¥.	VB	VĊ	011711 PL1234L TITC21 P3PNNP A		
0	-172	-217	-40	85	-17.0	-18.1	40.9	L**.		
Ö	-61	-24	-29	-9	26.6	-38.3	-1.2	LP*.		
0	444	460	13	-28	15.7	18.5	-40.6	L		
ŏ	17	14	4	1	-24.5	38.7	1.7	L1P. *.*.*		
ŏ	-556	-562	-2	5	-15.4	-18.6	40.5	L.31P. *.*.**.		
õ	- 13	-12	ō	0	24.2	-38.8	-1.7	L.31P. *.*.*		
0	571	575	0	- 1	15.4	18.6	-40.5	L.31P. *.*.*		
ŏ	13	11	Q	-1	-24.2	38.8	1.7	L.31P. *.*.*		
ŏ	-574	-576	Ö	1	-15.3	-18.6	40.5	L.31P. *.*.*.,		
ŏ	-12	-12	ō	1	24.2	-38.8	-1.8	L.31P. *.*.*		
							-			

Location : 29.97 mi 3.76 ohms sec Event : 1AG Duration: 7.25 Fit Current: 576.8

Currents and voltages art in primary Amps and KV. Rows are 1/4 cycle apart. Time runs down page. Obtain phasor RMS value and angle using any entry as Y-component, and the entry immediately underneath as the X-component. For example, from the middle rows, LAY = -562, LAX = -12. Therefore, LA = 562 amps RMS primary, at an angle of ATAN(-562/-12) = -91 degrees, with respect to the sampling clock.

<Relays> columns show states of internal relay elements ---> Designators

<Outputs> columns show states of output contacts: ON = *** , OFF = "."

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1 13 one of AG,8G,CG = single-phase, AB,8C,CA = 2-phase ABG,BCG,CAG = 2-phase to ground, ABC = 3-phase followed by a *T* if a TRIP triggered the report Other indications are TRIP = triggered by TRIP output

and i	EXT =	exter	natty (pr at	herwise	trigge	red

	AND EXT - EXCEPTIALLY OF ULTERWISE CITIEST
<location></location>	Distance to fault in miles. 999999 is indeterminate distance
<ohns sec=""></ohns>	Distance to fault in secondary ohms. 999999 is indeterminate
<duration></duration>	Fault duration determined from relay element(s) pickup time
«Fit Current»	Max phase current (primary amps) taken near middle of fault
R1, X1, R0, X0	Primary series impedance settings for transmission line
LL	line length corresponding to specified line impedances
CTR, PTR	Current and potential transformer ratios (XTR:1)
HTA	Maximum torque angle for mho elements
LOCAT	Frable or disable fault locator (Y/N)
47PXD,47PXL	Positive sequence voltage, dead voltage/live voltage threshold
vct	Voltage condition timer
LLC,DLC	Live voltage/Dead voltage supervision
CVC	Valtage supervision required at close
VSA	All shots/first shot only with voltage supervision
79011,2,3,RS	Three-shot recloser Open and Reset intervals
50L,50H	Phase fault detector and high-set instantaneous settings
218,228,238	Reaches of 3- and 2-phase mhos, percent of (ine length (LL)
2309	Zone 3 timer setting for 3- and 2-phase faults
SIPP, TD,C	PHASE time-overcurrent Pickup, Time-Dial, Curve
SINP, TD, C, TC	CND rime-overcurrent Pickup, Time-Disl, Curve, Torque Control
50N1P,2,3	Ground inst-overcurrent pickup settings zones 1, 2, and 3
220G, 23DG	Zone 2 and 3 timers for ground faults
528T	528 delay setting (for switch-onto-fault coordination)
ZONE3	Directional orientation of ALL zone 3 elements (Fwd/RVs)
320E, VE, 1E	Ground fault directionality from (V2,I2), or (V0/1P,10)
LOPE	For the for the of Potential SUCCEVISION (Y/N)
TIME1,2	Communications port timeout intervais (automatic log-off)
AUTO	Port essignment for automatic message transmissions
DINCE	Number of right to wait before modern answers telephone
donie sattit	ngs> See LOGIC command for a description of mask setting.
PARIS ACTOR	·œ ··· ··· ·

SAMPLE COMMAND DISPLAYS

=>>HISTORY

The date, time, and type of event are shown for each of the twelve most recent events. If the event is a fault, the distance, duration, and current are shown. An example of the display is shown below:

Example 69kV	Line			Date: 2/28/87	Time: 01:45:40
 # DATE 1 2/28/87 2 2/28/87 3 2/28/87 4 2/28/87 5 6 7 8 9 10 11 12 	TIME 09:03:01.092 09:02:13.041 09:00:39.962 09:00:13.345	TYPE 3AGT 3ABC 1AG 1BC	DIST 94.45 95.09 9.02 9.05	DUR CURR 11.00 365.6 7.00 364.7 7.25 1150.3 7.25 1324.0	

Note that only four events have occurred since the relay was set or powered on.

=>>METER

Example 69	kV Line			Date: 2,	Time	: 13:27:05	
1 (A) V (kV)	A 220 40.2	B 221 40.2	C 219 40.2	AB 381 69.6	BC 381 69.5	CA 380 69.7	
P (MW) Q (MVAR)	26.40 0.25						

P and Q are positive when the power flow is in the direction of the reach of the relay, i.e., out from the bus and into the line.

=>>STATUS

Example 69kV Line

Date: 2/28/87

Time: 01:04:56

SELF-TESTS

W=Warn F=Fail

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	IP	IR	IA	IB	IC	VA	٧B	VC
0S	0	0	2	2	4	-2	-2	-2
PS	4.9	99	15.	14	-14	. 85		
RAM	RO	1	A/D	MOF		SET		
0K	OK		ΟK	OK	(Ж		

=>>TARGETS

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The eight-LED display on the front panel can be programmed to show targets (default), Relay Word bits, contact inputs and contact outputs, as shown below. This feature is especially useful for testing individual relay elements.

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LED:	1	2	3	4	5	6	7	8	
N									
0	EN	PH1	G1	PH2	G2	РНЗ	G3	51N	RELAY TARGETS
1	51PT	1ABC	2ABC	3ABC	51PP	50H	50L	LOP	RELAY WORD #1
2	51NT	67N1	67N2	67N3	51NP	Z1P	Z2P	Z3P	RELAY WORD #2
3	DF	DR	Z2GT	Z3GT	3P50	RC	RI	Z3PT	RELAY WORD #3
4	ALRM	TRIP	TC	DT	52BT	52AT			RELAY WORD #4
5	52AT		ET	52A	DC	BT	РТ	DT	CONTACT INPUTS
6		TRIP	CLOS	A1	A2	A3	A4	ALRM	CONTACT OUTPUTS

The front panel targets can be reset and cleared remotely or locally using the target command. Type "TARGET R <RETURN>" to reset and clear the targets.

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DMG. NO. A7-0463 DATE: 10-04-86



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DWG. NO. A7-0339 DATE: 08-24-88



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DWG. ND. A7-0333 DATE: C8-19-58





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DWG, NO, A7-0401 DATE: 10-12-83

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SEL-121C COMMUNICATIONS AND CLOCK CONNECTIONS ONE UNIT AT ONE LOCATION

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DWG. NO. A7-0330 DATE: 38-19-88

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DWG. NO. A7-0413 DATE: 10-07-88

RELAY COMMUNICATIONS DIAGRAM FOR CONNECTION TO THE SEL-DIA SEL

NOTE: SEL-DTA DISPLAY/TRANSDUCER ADAPTER (DTA) DATA AND CONTROL POWER





NOTICE OF PROPRIETARY INFORMATION

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DWG. NJ. A7-0334 DATE: 08-18-88

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SEL-121C HORIZONTAL REAR PANEL DRAWING

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DWG. NO. A7-0335 DATE: 08-19-88



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SEL-121C VERTICAL REAR PANEL DRAWING

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> DWG. NO. A7-0402 DATE: 09-30-88



- DIMENSION A: CASE: 17.00" CUT OUT: 17.25" - 17.875" 17.375" PREFERRED DIMENSION B: CASE: 8.5" CUT OUT: 8.625" - 8.9375" 8.688" PREFERRED DIMENSION C:
- CASE: 5.25" CUT OUT:5.35" - 5.45" DIMENSION D: CASE: 2.625" CUT OUT: 2.675" - 2.725"
- <u>NOTE:</u> ALL INSTRUMENTS MAY BE MOUNTED HORIZONTALLY (AS SHOWN) OR VERTICALLY.

PANEL CUTOUT AND DRILL PLAN FOR SEMI-FLUSH MOUNTING OF 5.25 INCH HIGH CASE

DWG. NO. A7-0174 DATE 5/11/87 JS REV. 3/9/88

<u>Leve] O</u>	
ACCESS	Answer password prompt (if password protection enabled) to gain access to Level 1. Three unsuccessful attempts pulses ALARM relay.
<u>Level 1</u>	
2ACCESS	Answer password prompt (if password protection enabled) to gain
DATE	access to Level 2. This command always pulses the ALARM relay. Show or set date. DAT 2/3/86 sets date to Feb. 3, 1986. This setting is overridden when IRIG-B synchronization occurs. Pulses the ALARM momentarily when a different year is entered than the one previously stored.
EVENT HISTORY	Show event record. EVE 1 shows long form of most-recent event. Show DATE, TIME, EVENT TYPE, FAULT LOCATION, DURATION, and CURRENT for the 12 most recent faults.
IRIG METER	Force immediate execution of time-code synchronization task. Show primary current, voltage, real and reactive power. METER runs once. METER N runs N times
QUIT SHOWSET	Return to Access Level 0. Show the relay settings and logic settings does not affect the settings. The logic settings are shown in hexadecimal format for each.
STATUS TARGETS	Show self-test status. Show data and set target lights as follows: TAR 0: Relay Targets TAR 1: RELAY WORD #1 TAR 2: RELAY WORD #2 TAR 3: RELAY WORD #3 TAR 4: RELAY WORD #4 TAR 5: Contact Inputs TAR 6: Contact Outputs TAR R: Returns to TAR 0 and clears Be sure to return to TAR 0 when done, so LEDs display fault targets.
TIME	Show or set time. TIM 13:32:00 sets clock to 1:32:00 PM. This setting is overridden when IRIG-B synchronization occurs.
TRIGGER	Trigger and save an event record. (Type of event is EXT).
<u>Level 2</u>	
CLOSE LOGIC* OPEN PASSWORD	Close circuit breaker, if allowed by jumper setting. Show or set logic masks MTU, MPT, MTO, MTB, MRI, MRC, MA1-MA4. Open circuit breaker, if allowed by jumper setting. Show or set passwords. Pulses the ALARM momentarily when new passwords are set. PAS 1 OTTER sets Level 1 password to OTTER. PAS 2 TAIL sets Level 2 password to TAIL.
SET*	Initiate setting procedure.
	llowing to separate commands and their parameters: ma, semicolon, colon, slash.
	lay closes momentarily while new settings are being computed and ta buffers are cleared.

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